

SET-3G™ High-Strength Epoxy Adhesive

SET-3G is the latest innovation in epoxy anchoring adhesives with high design strength and proven performance. SET-3G is a 1:1 ratio, two-component, anchoring adhesive for concrete (cracked and uncracked). SET-3G installs and performs in a variety of environmental conditions and temperature extremes.

Features

- Exceptional performance — superior bond strengths permit ductile solutions in high seismic areas
- Design flexibility — improved sustained load performance at elevated temperature
- Jobsite versatility — can be specified for all base material conditions when in-service temperatures range from -40°F (-40°C) to 176°F (80°C)
- Recognized per ICC ES AC308 for post-installed rebar development and splice length design provisions
- Code listed for installation with the Speed Clean™ DXS, dustless drilling system without further hole cleaning

Product Information

| | |
|--|------------------------------------|
| Mix Ratio/Type | 1:1 epoxy |
| Mixed Color | Gray |
| Base Materials | Concrete — cracked and uncracked |
| Base Material Conditions | Dry, water-saturated, water-filled |
| Anchor Type | Threaded rod or rebar |
| Substrate Installation Temperature | 40°F (4°C) to 100°F (38°C) |
| In-Service Temperature Range | -40°F (-40°C) to 176°F (80°C) |
| Storage Temperature | 45°F (7°C) and 90°F (32°C) |
| Shelf Life | 24 months |
| Volatile Organic Compound (VOC) | 2 g/L |
| Chemical Resistance | See pp. 268–269 |
| Manufactured in the USA using global materials | |

Test Criteria

SET-3G has been tested in accordance with ICC-ES AC308, ACI 355.4 and applicable ASTM test methods.

Code Reports, Standards and Compliance

Concrete — ICC-ES ESR-4057 (including post-installed rebar connections and City of LA); FL15730.

Masonry — coming 2021.

ASTM C881 and AASHTO M235 — Types I/IV and II/IV, Grade 3, Class B & C.

UL Certification — CDPH Standard Method v1.2.

NSF/ANSI/CAN 61 (216 in.² / 1,000 gal.).

SET-3G Adhesive Cartridge System

| Model No. | Capacity (ounces) | Cartridge Type | Carton Quantity | Dispensing Tool(s) | Mixing Nozzle ³ |
|------------------------|-------------------|----------------|-----------------|-------------------------------|----------------------------|
| SET3G10 ¹ | 8.5 | Coaxial | 12 | CDT10S | EMN22I |
| SET3G22-N ¹ | 22 | Side-by-side | 10 | EDT22S, EDTA22P, EDTA22CKT | |
| SET3G56 | 56 | Side-by-side | 6 | EDTA56P | |

1. One EMN22I mixing nozzle and one extension are supplied with each cartridge.

2. Cartridge estimation guidelines are available at strongtie.com/softwareandwebapplications/category.

3. Use only Simpson Strong-Tie® mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair SET-3G adhesive performance.

4. Use of rodless pneumatic tools to dispense single-tube, coaxial adhesive cartridges is prohibited.



SET-3G Adhesive

Installation Instructions

Installation instructions are located at the following locations: pp. 64–67; product packaging; or strongtie.com/set3g.

- Hole cleaning brushes are located on p. 68.

SET-3G™ High-Strength Epoxy Adhesive

SET-3G Cure Schedule^{1,2}

| Concrete Temperature | | Gel Time | Cure Time |
|----------------------|------|----------|-----------|
| (°F) | (°C) | (min.) | (hr.) |
| 40 | 4 | 120 | 192 |
| 50 | 10 | 75 | 72 |
| 60 | 16 | 50 | 48 |
| 70 | 21 | 35 | 24 |
| 90 | 32 | 25 | 24 |
| 100 | 38 | 15 | 24 |

For SI: 1°F = (°C x 9/5) + 32.

- For water-saturated concrete and water-filled holes, the cure times shall be doubled.
- For installation of anchors in concrete where the temperature is below 70°F (21°C), the adhesive must be conditioned to a minimum temperature of 70°F (21°C).

SET-3G Typical Properties

| Property | | Class B | Class C | Test Method |
|--|---|----------------------------------|-------------|-------------|
| | | (40°–60°F) | (> 60°F) | |
| Consistency | | Non-sag | Non-sag | ASTM C881 |
| Bond Strength, Slant Shear | Hardened to Hardened Concrete, 2-Day Cure ¹ | 3,700 psi | 3,300 psi | ASTM C882 |
| | Hardened to Hardened Concrete, 14-Day Cure ¹ | 3,850 psi | 3,350 psi | |
| | Fresh to Hardened Concrete, 14-Day Cure ² | 2,750 psi | 2,750 psi | |
| Compressive Yield Strength, 7-Day Cure ² | | 13,000 psi | 15,350 psi | ASTM D695 |
| Compressive Modulus, 7-Day Cure ² | | 650,000 psi | 992,000 psi | ASTM D695 |
| Heat Deflection Temperature, 7-Day Cure ² | | 147°F (64°C) | | ASTM D648 |
| Glass Transition Temperature, 7-Day Cure ² | | 149°F (65°C) | | ASTM E1356 |
| Decomposition Temperature, 24-Hour Cure ² | | 500°F (260°C) | | ASTM E2550 |
| Water Absorption, 24-Hours, 7-Day Cure ² | | 0.13% | | ASTM D570 |
| Shore D Hardness, 24-Hour Cure ² | | 84 | | ASTM D2240 |
| Linear Coefficient of Shrinkage, 7-Day Cure ² | | 0.002 in./in. | | ASTM D2566 |
| Coefficient of Thermal Expansion ² | | 2.3 x 10 ⁻⁵ in./in.°F | | ASTM C531 |

- Material and curing conditions: Class B at 40° ± 2°F, Class C at 60° ± 2°F.
- Material and curing conditions: 73° ± 2°F.

SET-3G Installation Information and Additional Data for Threaded Rod and Rebar¹



| Characteristic | Symbol | Units | Nominal Anchor Diameter d_a (in.) / Rebar Size | | | | | | |
|-------------------------------------|---------------|---------|--|----------|----------|----------------------|----------|--------|-------------|
| | | | 3/8 / #3 | 1/2 / #4 | 5/8 / #5 | 3/4 / #6 | 7/8 / #7 | 1 / #8 | 1 1/4 / #10 |
| Installation Information | | | | | | | | | |
| Drill Bit Diameter for Threaded Rod | d_{hole} | in. | 7/16 | 9/16 | 1 1/16 | 7/8 | 1 | 1 1/8 | 1 3/8 |
| Drill Bit Diameter for Rebar | d_{hole} | in. | 1/2 | 5/8 | 3/4 | 7/8 | 1 | 1 1/8 | 1 3/8 |
| Maximum Tightening Torque | T_{inst} | ft.-lb. | 15 | 30 | 60 | 100 | 125 | 150 | 200 |
| Minimum Embedment Depth | $h_{ef, min}$ | in. | 2 3/8 | 2 3/4 | 3 1/8 | 3 1/2 | 3 3/4 | 4 | 5 |
| Maximum Embedment Depth | $h_{ef, max}$ | in. | 7 1/2 | 10 | 12 1/2 | 15 | 17 1/2 | 20 | 25 |
| Minimum Concrete Thickness | h_{min} | in. | $h_{ef} + 1 1/4$ | | | $h_{ef} + 2d_{hole}$ | | | |
| Critical Edge Distance | c_{ac} | in. | See footnote 2 | | | | | | |
| Minimum Edge Distance | c_{min} | in. | 1 3/4 | | | | | | 2 3/4 |
| Minimum Anchor Spacing | s_{min} | in. | 1 | 2 1/2 | 3 | | | 6 | |

1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.

2. $c_{ac} = h_{ef} (\tau_{k, uncr} / 1,160)^{0.4} \times [3.1 - 0.7(h/h_{ef})]$, where:
 $[h/h_{ef}] \leq 2.4$

$\tau_{k, uncr}$ = the characteristic bond strength in uncracked concrete, given in the tables that follow $\leq k_{uncr} ((h_{ef} \times f'_c)^{0.5} / (\pi \times d_a))$

h = the member thickness (inches)

h_{ef} = the embedment depth (inches)

d_a = nominal anchor diameter

* See p. 12 for an explanation of the load table icons.

SET-3G™ Design Information — Concrete

SET-3G Tension Strength Design Data for Threaded Rod^{1,8}



| Characteristic | | Symbol | Units | Nominal Rod Diameter (in.) | | | | | | | | |
|---|------------------------------------|---|--|----------------------------|-----------------|--------|--------------------|--------------------|--------|---------|-------|-------|
| | | | | 3/8 | 1/2 | 5/8 | 3/4 | 7/8 | 1 | 1 1/4 | | |
| Steel Strength in Tension | | | | | | | | | | | | |
| Minimum Tensile Stress Area | | A_{se} | in. ² | 0.078 | 0.142 | 0.226 | 0.334 | 0.462 | 0.606 | 0.969 | | |
| Tension Resistance of Steel — ASTM F1554, Grade 36 | | N_{sa} | lb. | 4,525 | 8,235 | 13,110 | 19,370 | 26,795 | 35,150 | 56,200 | | |
| Tension Resistance of Steel — ASTM F1554, Grade 55 | | | | 5,850 | 10,650 | 16,950 | 25,050 | 34,650 | 45,450 | 72,675 | | |
| Tension Resistance of Steel — ASTM A193, Grade B7 | | | | 9,750 | 17,750 | 28,250 | 41,750 | 57,750 | 75,750 | 121,125 | | |
| Tension Resistance of Steel — Stainless Steel ASTM A193, Grade B8 and B8M (Types 304 and 316) | | | | 4,445 | 8,095 | 12,880 | 19,040 | 26,335 | 34,540 | 55,235 | | |
| Tension Resistance of Steel — Stainless Steel ASTM F593 CW (Types 304 and 316) | | | | 7,800 | 14,200 | 22,600 | 28,390 | 39,270 | 51,510 | 82,365 | | |
| Tension Resistance of Steel — Stainless Steel ASTM A193, Grade B6 (Type 410) | | | | 8,580 | 15,620 | 24,860 | 36,740 | 50,820 | 66,660 | 106,590 | | |
| Strength Reduction Factor for Tension — Steel Failure | | ϕ | — | 0.75 ⁵ | | | | | | | | |
| Concrete Breakout Strength in Tension (2,500 psi ≤ f_c ≤ 8,000 psi) | | | | | | | | | | | | |
| Effectiveness Factor for Cracked Concrete | | $k_{c,cr}$ | — | 17 | | | | | | | | |
| Effectiveness Factor for Uncracked Concrete | | $k_{c,uncr}$ | — | 24 | | | | | | | | |
| Strength Reduction Factor — Concrete Breakout Failure in Tension | | ϕ | — | 0.65 ⁶ | | | | | | | | |
| Bond Strength in Tension (2,500 psi ≤ f_c ≤ 8,000 psi)⁷ | | | | | | | | | | | | |
| Minimum Embedment | | $h_{ef,min}$ | in. | 2 3/8 | 2 3/4 | 3 1/8 | 3 1/2 | 3 3/4 | 4 | 5 | | |
| Maximum Embedment | | $h_{ef,max}$ | in. | 7 1/2 | 10 | 12 1/2 | 15 | 17 1/2 | 20 | 25 | | |
| Continuous Inspection | Temperature Range A ^{2,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | | $\tau_{k,cr}$ | psi | 1,448 | 1,402 | 1,356 | 1,310 | 1,265 | 1,219 | 1,128 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | | $\tau_{k,uncr}$ | psi | 2,357 | 2,260 | 2,162 | 2,064 | 1,967 | 1,868 | 1,672 |
| | Temperature Range B ^{3,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | | $\tau_{k,cr}$ | psi | 1,201 | 1,163 | 1,125 | 1,087 | 1,050 | 1,012 | 936 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | | $\tau_{k,uncr}$ | psi | 1,957 | 1,876 | 1,795 | 1,713 | 1,632 | 1,551 | 1,388 |
| | Anchor Category | | Dry Concrete | | — | — | 1 | | | | | |
| | Strength Reduction Factor | | Dry Concrete | | $\phi_{dry,ci}$ | — | 0.65 ¹⁰ | | | | | |
| | Anchor Category | | Water-Saturated Concrete, or Water-Filled Hole | | — | — | 3 | 2 | | | | |
| | Strength Reduction Factor | | Water-Saturated Concrete, or Water-Filled Hole | | $\phi_{wet,ci}$ | — | 0.45 ¹⁰ | 0.55 ¹⁰ | | | | |
| Periodic Inspection | Temperature Range A ^{2,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | | $\tau_{k,cr}$ | psi | 1,346 | 1,304 | 1,356 | 1,310 | 1,265 | 1,219 | 1,128 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | | $\tau_{k,uncr}$ | psi | 2,192 | 2,102 | 2,162 | 2,064 | 1,967 | 1,868 | 1,672 |
| | Temperature Range B ^{3,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | | $\tau_{k,cr}$ | psi | 1,117 | 1,082 | 1,125 | 1,087 | 1,050 | 1,012 | 936 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | | $\tau_{k,uncr}$ | psi | 1,820 | 1,744 | 1,795 | 1,713 | 1,632 | 1,551 | 1,388 |
| | Anchor Category | | Dry Concrete | | — | — | 2 | 1 | | | | |
| | Strength Reduction Factor | | Dry Concrete | | $\phi_{dry,pi}$ | — | 0.55 ¹⁰ | 0.65 ¹⁰ | | | | |
| | Anchor Category | | Water-Saturated Concrete, or Water-Filled Hole | | — | — | 3 | | | | | |
| | Strength Reduction Factor | | Water-Saturated Concrete, or Water-Filled Hole | | $\phi_{wet,pi}$ | — | 0.45 ¹⁰ | | | | | |
| Reduction Factor for Seismic Tension | | $\alpha_{N,seis}$ ¹¹ | — | 1.0 | 0.9 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | |

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.
- Temperature Range A: Maximum short-term temperature = 160°F, maximum long-term temperature = 110°F.
- Temperature Range B: Maximum short-term temperature = 176°F, maximum long-term temperature = 110°F.
- Short-term concrete temperatures are those that occur over short intervals (diurnal cycling). Long-term temperatures are roughly constant over significant periods of time.
- The tabulated value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- The tabulated value of ϕ applies when both the load combinations of ACI 318-14 5.3, or ACI 318-11 9.2 are used and the requirements of ACI 318-14 17.3.3 (c) or ACI 318-11 D.4.3 (c), as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318 D.4.4 (c) for Condition B to determine the appropriate value of ϕ .
- Bond strength values shown are for normal-weight concrete having a compressive strength of $f'_c = 2,500$ psi. For higher compressive strengths up to 8,000 psi, the tabulated characteristic bond strength may be increased by a factor of $(f'_c/2,500)^{0.35}$ for uncracked concrete and a factor of $(f'_c/2,500)^{0.24}$ for cracked concrete.
- For lightweight concrete, the modification factor for bond strength shall be as given in ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable, where applicable.
- Characteristic bond strength values are for sustained loads, including dead and live loads.
- The tabulated value of ϕ applies when both the load combinations of ACI 318-14 5.3, or ACI 318-11 9.2 are used and the requirements of ACI 318-14 17.3.3 (c) or ACI 318-11 D.4.3 (c), as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318 D.4.4(c) for Condition B to determine the appropriate value of ϕ .
- For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values must be multiplied by $\alpha_{N,seis}$.

* See p. 12 for an explanation of the load table icons.

SET-3G™ Design Information — Concrete

SET-3G Tension Strength Design Data for Rebar^{1,8}



| Characteristic | | Symbol | Units | Rebar Size | | | | | | | |
|---|------------------------------------|---|--|-------------------|--------------------|--------|--------|--------------------|--------|---------|-------|
| | | | | #3 | #4 | #5 | #6 | #7 | #8 | #10 | |
| Steel Strength in Tension | | | | | | | | | | | |
| Minimum Tensile Stress Area | | A_{se} | in. ² | 0.11 | 0.20 | 0.31 | 0.44 | 0.60 | 0.79 | 1.27 | |
| Tension Resistance of Steel — Rebar (ASTM A615 Grade 60) | | N_{sa} | lb. | 9,900 | 18,000 | 27,900 | 39,600 | 54,000 | 71,100 | 114,300 | |
| Tension Resistance of Steel — Rebar (ASTM A706 Grade 60) | | | | 8,800 | 16,000 | 24,800 | 35,200 | 48,000 | 63,200 | 101,600 | |
| Strength Reduction Factor for Tension — Steel Failure | | ϕ | — | 0.75 ⁹ | | | | | | | |
| Concrete Breakout Strength in Tension (2,500 psi ≤ f'_c ≤ 8,000 psi) | | | | | | | | | | | |
| Effectiveness Factor for Cracked Concrete | | $k_{c,cr}$ | — | 17 | | | | | | | |
| Effectiveness Factor for Uncracked Concrete | | $k_{c,uncr}$ | — | 24 | | | | | | | |
| Strength Reduction Factor — Concrete Breakout Failure in Tension | | ϕ | — | 0.65 ⁹ | | | | | | | |
| Bond Strength in Tension (2,500 psi ≤ f'_c ≤ 8,000 psi)⁷ | | | | | | | | | | | |
| Minimum Embedment | | $h_{ef,min}$ | in. | 2¾ | 2¾ | 3⅞ | 3½ | 3¾ | 4 | 5 | |
| Maximum Embedment | | $h_{ef,max}$ | in. | 7½ | 10 | 12½ | 15 | 17½ | 20 | 25 | |
| Continuous Inspection | Temperature Range A ^{2,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | $\tau_{k,cr}$ | psi | 1,448 | 1,402 | 1,356 | 1,310 | 1,265 | 1,219 | 1,128 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | $\tau_{k,uncr}$ | psi | 2,269 | 2,145 | 2,022 | 1,898 | 1,774 | 1,651 | 1,403 |
| | Temperature Range B ^{3,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | $\tau_{k,cr}$ | psi | 1,201 | 1,163 | 1,125 | 1,087 | 1,050 | 1,012 | 936 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | $\tau_{k,uncr}$ | psi | 1,883 | 1,781 | 1,678 | 1,575 | 1,473 | 1,370 | 1,165 |
| | Anchor Category | | Dry Concrete | — | 1 | | | | | | |
| | Strength Reduction Factor | | Dry Concrete | $\phi_{dry,ci}$ | 0.65 ¹⁰ | | | | | | |
| | Anchor Category | | Water-Saturated Concrete, or Water-Filled Hole | — | 3 | | | 2 | | | |
| | Strength Reduction Factor | | Water-Saturated Concrete, or Water-Filled Hole | $\phi_{wet,ci}$ | 0.45 ¹⁰ | | | 0.55 ¹⁰ | | | |
| Periodic Inspection | Temperature Range A ^{2,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | $\tau_{k,cr}$ | psi | 1,346 | 1,304 | 1,356 | 1,310 | 1,265 | 1,219 | 1,128 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | $\tau_{k,uncr}$ | psi | 2,110 | 1,995 | 2,022 | 1,898 | 1,774 | 1,651 | 1,403 |
| | Temperature Range B ^{3,4} | Characteristic Bond Strength in Cracked Concrete ⁹ | $\tau_{k,cr}$ | psi | 1,117 | 1,082 | 1,125 | 1,087 | 1,050 | 1,012 | 936 |
| | | Characteristic Bond Strength in Uncracked Concrete ⁹ | $\tau_{k,uncr}$ | psi | 1,751 | 1,656 | 1,678 | 1,575 | 1,473 | 1,370 | 1,165 |
| | Anchor Category | | Dry Concrete | — | 2 | | | 1 | | | |
| | Strength Reduction Factor | | Dry Concrete | $\phi_{dry,pi}$ | 0.55 ¹⁰ | | | 0.65 ¹⁰ | | | |
| | Anchor Category | | Water-Saturated Concrete, or Water-Filled Hole | — | 3 | | | | | | |
| | Strength Reduction Factor | | Water-Saturated Concrete, or Water-Filled Hole | $\phi_{wet,pi}$ | 0.45 ¹⁰ | | | | | | |
| Reduction Factor for Seismic Tension | | $\alpha_{N,seis}$ ¹¹ | — | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | |

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.
- Temperature Range A: Maximum short-term temperature = 160°F, maximum long-term temperature = 110°F.
- Temperature Range B: Maximum short-term temperature = 176°F, maximum long-term temperature = 110°F.
- Short-term concrete temperatures are those that occur over short intervals (diurnal cycling). Long-term temperatures are roughly constant over significant periods of time.
- The tabulated value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- The tabulated value of ϕ applies when both the load combinations of ACI 318-14 5.3, or ACI 318-11 9.2 are used and the requirements of ACI 318-14 17.3.3 (c) or ACI 318-11 D.4.3 (c), as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318 D.4.4(c) for Condition B to determine the appropriate value of ϕ .
- Bond strength values shown are for normal-weight concrete having a compressive strength of f'_c = 2,500 psi. For higher compressive strengths up to 8,000 psi, the tabulated characteristic bond strength may be increased by a factor of (f'_c/2,500)^{0.36} for uncracked concrete and a factor of (f'_c/2,500)^{0.25} for cracked concrete.
- For lightweight concrete, the modification factor for bond strength shall be as given in ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable, where applicable.
- Characteristic bond strength values are for sustained loads, including dead and live loads.
- The tabulated value of ϕ applies when both the load combinations of ACI 318-14 5.3, or ACI 318-11 9.2 are used and the requirements of ACI 318-14 17.3.3 (c) or ACI 318-11 D.4.3 (c), as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318 D.4.4(c) for Condition B to determine the appropriate value of ϕ .
- For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values must be multiplied by $\alpha_{N,seis}$.

* See p. 12 for an explanation of the load table icons.

SET-3G™ Design Information — Concrete

SET-3G Shear Strength Design Data for Threaded Rod¹

| Characteristic | Symbol | Units | Nominal Rod Diameter (in.) | | | | | | |
|---|-----------------------|------------------|--|--------|--------|--------|--------|--------|--------|
| | | | 3/8 | 1/2 | 5/8 | 3/4 | 7/8 | 1 | 1 1/4 |
| Steel Strength in Shear | | | | | | | | | |
| Minimum Shear Stress Area | A_{se} | in. ² | 0.078 | 0.142 | 0.226 | 0.334 | 0.462 | 0.606 | 0.969 |
| Shear Resistance of Steel — ASTM F1554, Grade 36 | V_{sa} | lb. | 2,715 | 4,940 | 7,865 | 11,625 | 16,080 | 21,090 | 33,720 |
| Shear Resistance of Steel — ASTM F1554, Grade 55 | | | 3,510 | 6,390 | 10,170 | 15,030 | 20,790 | 27,270 | 43,605 |
| Shear Resistance of Steel — ASTM A193, Grade B7 | | | 5,850 | 10,650 | 16,950 | 25,050 | 34,650 | 45,450 | 72,675 |
| Reduction factor for Seismic Shear — Carbon Steel | $\alpha_{V_{seis}}^4$ | — | 0.75 | | | | | 1.0 | |
| Shear Resistance of Steel — Stainless Steel ASTM A193, Grade B8 and B8M (Types 304 and 316) | V_{sa} | lb. | 2,665 | 4,855 | 7,730 | 11,425 | 15,800 | 20,725 | 33,140 |
| Shear Resistance of Steel — Stainless Steel ASTM F593 CW (Types 304 and 316) | | | 4,680 | 8,520 | 13,560 | 17,035 | 23,560 | 30,905 | 49,420 |
| Shear Resistance of Steel — Stainless Steel ASTM A193, Grade B6 (Type 410) | | | 5,150 | 9,370 | 14,915 | 22,040 | 30,490 | 40,000 | 63,955 |
| Reduction factor for Seismic Shear — Stainless Steel | $\alpha_{V_{seis}}^4$ | — | 0.80 | | 0.75 | | | 1.0 | |
| Strength Reduction Factor for Shear — Steel Failure | ϕ | — | 0.65 ² | | | | | | |
| Concrete Breakout Strength in Shear | | | | | | | | | |
| Outside Diameter of Anchor | d_a | in. | 0.375 | 0.5 | 0.625 | 0.75 | 0.875 | 1 | 1.25 |
| Load-Bearing Length of Anchor in Shear | l_e | in. | Min. of h_{ef} and 8 times anchor diameter | | | | | | |
| Strength Reduction Factor for Shear — Breakout Failure | ϕ | — | 0.70 ³ | | | | | | |
| Concrete Pryout Strength in Shear/ | | | | | | | | | |
| Coefficient for Pryout Strength | k_{cp} | in. | 1.0 for $h_{ef} < 2.50"$; 2.0 for $h_{ef} \geq 2.50"$ | | | | | | |
| Strength Reduction Factor for Shear — Breakout Failure | ϕ | — | 0.70 ³ | | | | | | |

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.
- The tabulated value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- The tabulated value of ϕ applies when both the load combinations of ACI 318-14 5.3, or ACI 318-11 9.2 are used and the requirements of ACI 318-14 17.3.3 (c) or ACI 318-11 D.4.3 (c), as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix B are used, refer to ACI 318 D.4.4 (c) for Condition B to determine the appropriate value of ϕ .
- The values of V_{sa} are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, V_{sa} must be multiplied by $\alpha_{V_{seis}}$ for the corresponding anchor steel type.

* See p. 12 for an explanation of the load table icons.

SET-3G™ Design Information — Concrete



SET-3G Shear Strength Design Data for Rebar¹

| Characteristic | Symbol | Units | Nominal Rod Diameter (in.) | | | | | | |
|---|-----------------------|------------------|--|--------|--------|--------|--------|--------|--------|
| | | | #3 | #4 | #5 | #6 | #7 | #8 | #10 |
| Steel Strength in Shear | | | | | | | | | |
| Minimum Shear Stress Area | A_{se} | in. ² | 0.110 | 0.200 | 0.310 | 0.440 | 0.600 | 0.790 | 1.270 |
| Shear Resistance of Steel — Rebar (ASTM A615 Grade 60) | V_{sa} | lb. | 5,940 | 10,800 | 16,740 | 23,760 | 32,400 | 42,660 | 68,580 |
| Shear Resistance of Steel — Rebar (ASTM A706 Grade 60) | | | 5,280 | 9,600 | 14,880 | 21,120 | 28,800 | 37,920 | 60,960 |
| Reduction Factor for Seismic Shear — Rebar (ASTM A615 Grade 60) | $\alpha_{V_{seis}}^A$ | — | 0.60 | | | | | | 0.8 |
| Reduction Factor for Seismic Shear — Rebar (ASTM A706 Grade 60) | | | 0.60 | | | | | | 0.8 |
| Strength Reduction Factor for Shear — Steel Failure | ϕ | — | 0.65 ² | | | | | | |
| Concrete Breakout Strength in Shear | | | | | | | | | |
| Outside Diameter of Anchor | d_a | in. | 0.375 | 0.5 | 0.625 | 0.75 | 0.875 | 1 | 1.25 |
| Load-Bearing Length of Anchor in Shear | l_e | in. | Min. of h_{ef} and 8 times anchor diameter | | | | | | |
| Strength Reduction Factor for Shear — Breakout Failure | ϕ | — | 0.70 ³ | | | | | | |
| Concrete Pryout Strength in Shear | | | | | | | | | |
| Coefficient for Pryout Strength | k_{cp} | in. | 1.0 for $h_{ef} < 2.50"$; 2.0 for $h_{ef} \geq 2.50"$ | | | | | | |
| Strength Reduction Factor for Shear — Breakout Failure | ϕ | — | 0.70 ³ | | | | | | |

- The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 and ACI 318-11.
- The tabulated value of ϕ applies when the load combinations of ACI 318-14 5.3 or ACI 318-11 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of ϕ .
- The tabulated value of ϕ applies when both the load combinations of ACI 318-14 5.3 or ACI 318-11 9.2 are used and the requirements of ACI 318-14 17.3.3 (c) or ACI 318-11 D.4.3 (c), as applicable, for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318 D.4.4 (c) for Condition B to determine the appropriate value of ϕ .
- The values of V_{sa} are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, V_{sa} must be multiplied by $\alpha_{V_{seis}}$ for the corresponding anchor steel type.

For additional load tables, visit strongtie.com/set3g.



Anchor Designer™ Software for ACI 318, ETAG and CSA

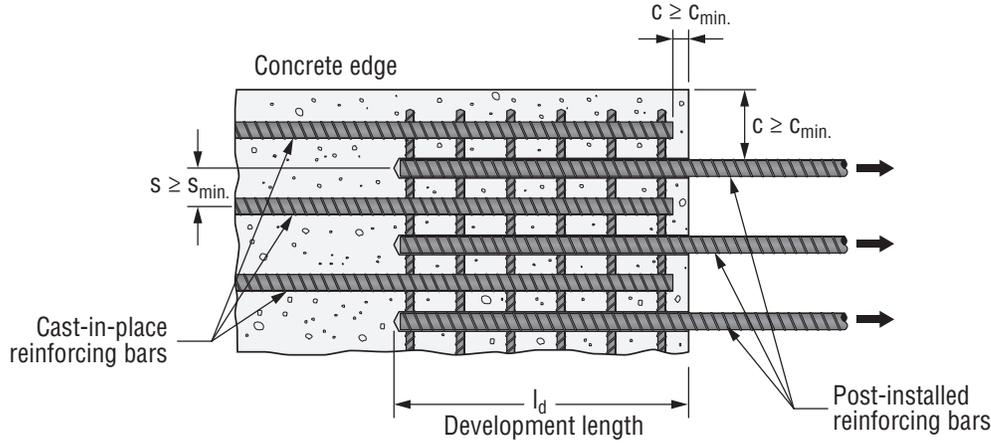
Simpson Strong-Tie® Anchor Designer software accurately analyzes existing design or suggests anchor solutions based on user-defined design elements in cracked and uncracked concrete conditions.

^{*} See p. 12 for an explanation of the load table icons.

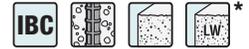
SET-3G™ Design Information — Concrete

SET-3G is code listed under IBC/IRC for cracked and uncracked concrete per ICC-ES ESR-4057.

In March 2020, the evaluation report was updated for SET-3G to be an equivalent to cast-in-place reinforcing bars governed by ACI 318 and IBC Chapter 19.



SET-3G Development Length for Rebar Dowel



| Rebar Size | Drill Bit Diameter (in.) | Clear Cover, in. (mm) | Development Length, in. (mm) | | | | |
|------------|--------------------------|-----------------------|--|--|--|--|--|
| | | | $f'_c = 2,500$ psi (17.2 MPa) Concrete | $f'_c = 3,000$ psi (20.7 MPa) Concrete | $f'_c = 4,000$ psi (27.6 MPa) Concrete | $f'_c = 6,000$ psi (41.4 MPa) Concrete | $f'_c = 8,000$ psi (55.2 MPa) Concrete |
| #3 | ½ | 1.125 (29) | 12 (305) | 12 (305) | 12 (305) | 12 (305) | 12 (305) |
| #4 | 5/8 | 1.125 (29) | 14.4 (366) | 14 (356) | 12 (305) | 12 (305) | 12 (305) |
| #5 | ¾ | 1.125 (29) | 18 (457) | 17 (432) | 14.2 (361) | 12 (305) | 12 (305) |
| #6 | 7/8 | 1.125 (29) | 21.6 (549) | 20 (508) | 17.1 (434) | 14 (356) | 13 (330) |
| #7 | 1 | 2.30 (58) | 31.5 (800) | 29 (737) | 25 (635) | 21 (533) | 18 (457) |
| #8 | 1 1/8 | 2.30 (58) | 36 (914) | 33 (838) | 28.5 (724) | 24 (610) | 21 (533) |
| #9 | 1 3/8 | 2.30 (58) | 40.5 (1,029) | 38 (965) | 32 (813) | 27 (686) | 23 (584) |
| #10 | 1 5/8 | 2.30 (58) | 45 (1,143) | 42 (1,067) | 35.6 (904) | 30 (762) | 26 (660) |
| #11 | 1 3/4 | 2.30 (58) | 51 (1,295) | 47 (1,194) | 41 (1,041) | 33 (838) | 29 (737) |

1. Tabulated development lengths are for static, wind and seismic load cases in Seismic Design Category A and B. Development lengths in Seismic Design Category C through F must comply with ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21, as applicable.
2. Rebar is assumed to be ASTM A615 Grade 60 or A706 ($f_y = 60,000$ psi). For rebar with a higher yield strength, multiply tabulated values by $f_y/60,000$ psi.
3. Concrete is assumed to be normal-weight concrete. For lightweight concrete, multiply tabulated values by 1.33.
4. Tabulated values assume bottom cover less than 12" cast below rebars ($\Psi_1 = 1.0$).
5. Uncoated rebar must be used.
6. The value of K_{tr} is assumed to be 0. Refer to ACI318-14 Section 25.4.2.3 or ACI 318-11 Section 12.2.3.

* See p. 12 for an explanation of the load table icons.