## Beam and Glulam Top-Flange Hangers

Designed to support large members typically found in glulam beam construction.
Material: Stirrup -7 gauge; LEG/MEG TF - 7 gauge; all other TF - 3 gauge
Finish: Simpson Strong-Tie gray paint. Some products available hot-dip galvanized or in black powder coat.

## Installation:

- Use all specified fasteners: see General Notes
- Maintain minimum 4D end distance and edge distance from bolt to end of header and nearest loaded edge per NDS requirements


## Options:

Skewed Seat - Top-Flange Models Only

- The LEG/MEG/EG series can be skewed up to $45^{\circ}$. The maximum allowable load is $10,000 \mathrm{lb}$. for LEG and MEG, 14,250 lb. for EG.


## Sloped Seat - Top-Flange Models Only

- The LEG/MEG/EG series can be sloped up to $45^{\circ}$. The maximum allowable load is $9,665 \mathrm{lb}$.; see illustration.
No Sloped and Skewed Combo Available.


## Offset Top Flange

- The LEG/MEG (only) top flange may be offset left or right for placement at the end of a header (see illustration). The maximum allowable load is $5,665 \mathrm{lb}$. (Min. $\mathrm{H}=11^{\prime \prime}$ for MEG, 9 " for LEG).
- No skews allowed on offset hangers.
- Models available without top flanges; see table loads.
Codes: See p. 11 for Code Reference Key Chart


LEG/MEG/EG Without Top Flange (see options)


LEG and MEG


EG with " H " dimension less than the face plate height. The EG's back plate is always $17^{1 / 2} 2^{\prime \prime}$, regardless of the stirrup height.


Typical LEG/MEG Top Flange Offset Left


Typical LEG Sloped Down Installation (MEG/EG similar)

| Joist or Purlin Size (in.) | Model No. | Dimensions (in.) |  |  |  |  | Min. Header Depth (in.) | Bolts |  |  |  | Allowable Loads |  |  |  |  |  | Code Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | W | Min. H | Max.H | TF |  | Header |  | Joist |  | Without Top Flange |  | Top Flange <br> No Triangle Theory |  | Top Flange Triangle Theory |  |  |
|  |  |  |  |  |  |  |  | Qty. | Dia. <br> (in.) | Qty. | Dia. <br> (in.) | Floor (100) | $\begin{aligned} & \text { Roof } \\ & \text { (125) } \end{aligned}$ | Floor <br> (100) | $\begin{aligned} & \text { Roof } \\ & \text { (125) } \end{aligned}$ | Floor (100) | Roof (125) |  |
| 31⁄8 LAM | LEG3 | 12 | $31 / 4$ | 9 | 331/2 | $21 / 2$ | 10 | 4 | $3 / 4$ | 2 | $3 / 4$ | 3,465 | 4,330 | 13,045 | 13,870 | 13,045 | 13,870 | $\begin{aligned} & \text { IBC, } \\ & \text { FL, LA } \end{aligned}$ |
| 51⁄8 LAM | LEG5 | 12 | $51 / 4$ | 9 | 321/2 | $21 / 2$ | 10 | 4 | $3 / 4$ | 2 | $3 / 4$ | 3,465 | 4,330 | 16,290 | 16,290 | 13,045 | 13,870 |  |
|  | MEG5 | 12 | $51 / 4$ | 9 | 321/2 | $21 / 2$ | 13 | 6 | $3 / 4$ | 2 | $3 / 4$ | 5,170 | 6,460 | 19,710 | 19,710 | 14,515 | 14,515 |  |
|  | EG5 | 113/4 | 51/4 | 11 | 321/2 | $21 / 2$ | 20 | 8 | 1 | 2 | 1 | 8,870 | 11,085 | 20,895 | 21,815 | 17,895 | 19,875 |  |
| 63/4 LAM | LEG7 | 12 | 67/8 | 9 | $311 / 2$ | $21 / 2$ | 10 | 4 | $3 / 4$ | 2 | $3 / 4$ | 3,465 | 4,330 | 16,290 | 16,290 | 13,045 | 13,870 |  |
|  | MEG7 | 12 | 67/8 | 9 | $311 / 2$ | $21 / 2$ | 13 | 6 | $3 / 4$ | 2 | $3 / 4$ | 5,170 | 6,460 | 19,710 | 19,710 | 14,515 | 14,515 |  |
|  | EG7 | 131/2 | 67/8 | 11 | $311 / 2$ | $21 / 2$ | 20 | 8 | 1 | 2 | 1 | 8,870 | 11,085 | 25,320 | 25,835 | 19,305 | 21,300 |  |
| 83/4 LAM | EG9 | 151/2 | 87/8 | 11 | 301/2 | $21 / 2$ | 20 | 8 | 1 | 2 | 1 | 8,870 | 11,085 | 25,320 | 25,835 | 20,895 | 22,895 |  |

1. Roof loads are $125 \%$ of floor loads unless limited by other criteria. Floor loads may be adjusted for load durations according to the code provided they do not exceed those in the roof column.
2. Allowable loads assume a carrying member width of $5 \frac{1}{1 / 8}$.
3. Specify H dimension.
4. Triangle Theory: Some code jurisdictions allow only half of the top-flange bearing area to be considered when performing a top-flange hanger calculation, as there is non-uniform stress under the top flange (presumed to be a triangular-shaped distribution). Therefore, loads are published above using the calculated "Triangle Theory." Loads are also published in the "No Triangle Theory" columns, which are based on calculations assuming full bearing on the top flange which do not exceed the tested value with a reduction factor of 3 .
