RCKW



Kneewall Connectors

This product is preferable to similar connectors because of (a) easier installation, (b) higher loads, (c) lower installed cost, or a combination of these features.

The Simpson Strong-Tie RCKW rigid connectors have been developed to resist overturning moment at the base of exterior kneewalls and parapets as well as interior partial-height walls. The RCKWS is a heavy 7-gauge stiffener that nests onto the RCKW clip. The screw holes and anchor holes in the stiffener line up with those in the RCKW clip, making fastener and anchor installation a snap. The RCKW clip and RCKWS stiffener are sold separately.

Features:

- Anchorage legs incorporate stiffened flanges, improving overturning moment resistance
- Large-diameter anchor hole accommodates ½"-diameter concrete screws and wedge anchors, such as the Titen HD® heavy-duty screw anchor and the Strong-Bolt® 2 wedge anchor
- For the RCKWS: 7-gauge stiffeners are secured to the RCKW clip with screws, optimizing overturning moment resistance and stiffness

Material: RCKW and RCKWS - 7 gauge

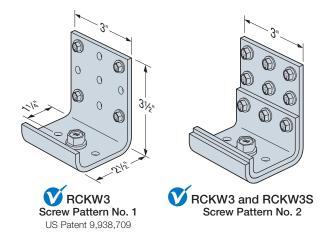
Coating: Galvanized

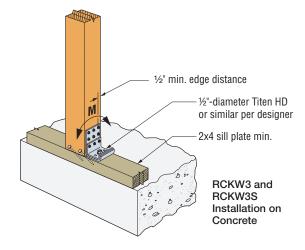
Installation:

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- · Use all specified screw fasteners.
- When using the RCKWS, secure the stiffener to the clip with the specified screw fasteners.
- Use all specified anchors. To achieve tabulated stiffness values, the installation torque for ½"-diameter anchors shall be at least 17 ft.-lb.
- For installation of the RCKW with 2x6 wood framing members, reference Simpson Strong-Tie engineering letter L-C-RCKW2X6WD at strongtie.com.

Codes: See p. 11 for Code Reference Key Chart





RCKW Allowable Loads for Wood Framing

Model No.	Screw Pattern No.	Fastener(s) to Post and Concrete	Nominal Post Size	Allowable Moment, M DF/SP (inlb.)	Anchor Tension, T, at Allow Moment, M (lb.)	$\begin{array}{c} \text{Assembly} \\ \text{Rotational} \\ \text{Stiffness} \\ \beta \\ \text{(inlb./rad.)} \end{array}$	$\begin{array}{c} \text{Connector} \\ \text{Rotational} \\ \text{Stiffness} \\ \beta_{\text{C}} \\ \text{(inlb/rad.)} \end{array}$	
RCKW3	1	(4) #10 x 21/2" SD (1) 1/2" Ø Anchor	(2) 2x4 or 4x4	2,165	1,695	102.800	111,300	
RCKW3 RCKW3S	2	(9) #10 x 21/2" SD (1) 1/2" Ø Anchor	(2) 2x4 or 4x4	3,725	3,635	102,000		

- 1. Designer is responsible for anchorage and framing member design.
- 2. Tabulated values are based on wood post connected to sill plate in accordance with the fastening schedule IBC Section 2304.
- 3. Multiply allowable moment and stiffness with an adjustment factor of 0.86 when attaching RCKW connector to SPF/HF wood post.
- 4. Anchor Tension, T, is the force in the anchor at allowable moment and is based on minimum concrete compressive strength, f'c of 2500 spi.
- 5. Tabulated Allowable Moment values correspond to connector strength without consideration of serviceability. Designer must check out-of-plane deflections using tabulated rotational stiffness values.
- 6. Tabulated Assembly Rotational Stiffness is applicable for studs up to 38" tall and includes connector deflection, fastener slip and bending in the stud. For framing members greater than 38" tall, the designer must consider member deflection due to bending in the stud member in addition to the tabulated Connector Rotational Stiffness. See flier F-CF-RCKW at strongtie.com for calculation example.
- Tabulated rotational stiffness values may be increased by dividing by a factor of 0.42 for deflection checks using component and cladding wind loads in lieu of reducing loads in accordance with 2012, 2015, 2018 and 2021 IBC Table 1604.3.
- 8. Built-up post (multiple members) must be fastened together to act as one unit to resist the applied load (excluding the connector fasteners). This must be determined by the designer.
- Anchor bolt nut should be finger tight plus 1/2 to 1/2 turn with a hand wrench, with consideration given to possible wood shrinkage.Moisture content of wood sill plate shall not exceed 19% at time of installation.
- 10. Fasteners: SD screws are Simpson Strong-Tie® Strong-Drive® SD Connector screws. See pp. 21-22 for fastener information.



This product is preferable to similar connectors because of a) easier installation, b) higher loads, c) lower installed cost, or a combination of these features.

The Simpson Strong-Tie® RCKW is a heavy 171 mil (7 ga.) rigid connector that has been developed to resist an overturning moment at the base of exterior kneewalls and parapets as well as interior partial-height walls or overhead ribbon window conditions. These connectors offer a unique small and large anchor-hole pattern that permits anchorage to both concrete and structural steel. The single-anchor RCKW has been redesigned to have all of the same features as the previous model but with an added two-anchor option that accommodates ½"- or ¾"-diameter concrete anchors. If load requires more capacity, a stiffener, the RCKWS can be added. The RCKWS is a heavy 171 mil (7 ga.) stiffener that nests onto the RCKW clip. The screw holes and anchor holes in the stiffener line up with those in the RCKW clip, making fastener and anchor installation a snap. The RCKW clip and RCKWS stiffener are sold separately.

Features

- Anchorage legs incorporate stiffened flanges, improving overturning moment resistance.
- Large-diameter anchor holes accommodate ½"-diameter concrete screw anchor and wedge anchors, such as the Simpson Strong-Tie Titen HD® heavy-duty screw anchor and the Strong-Bolt® 2 wedge anchor.
- The RCKW5.5 and RCKW7.5 have three large holes for added versatility. The center large hole is for a one-anchor solution at the edge or center of slab. The outer larger holes are for a two-anchor solution that requires higher capacities at the center of slab. In addition, two %" Titen HD screw anchors have been tested in the outer larger holes for shallower embedment required conditions like fluted deck.
- Additional smaller-diameter anchor holes enable attachment to structural steel with #12 self-drilling screws.
- Attachment to CMU can be achieved with Titen HD or Titen® 2 concrete and masonry screws.
- For the RCKWS: 171 mil (7 ga.) stiffeners are secured to the RCKW clip with screws, optimizing overturning moment resistance and stiffness.

Material: RCKW and RCKWS - 171 mil (7 ga.), 33 ksi

Coating: Galvanized (G90)

Installation:

- Use all specified screw fasteners. To achieve tabulated load values, use #12–14 screws according to the fastener patterns on p. 105.
- When using the RCKWS, secure the stiffener to the clip with the specified screw fasteners. Screws must be at least 1" long and extend through the connection with a minimum of three exposed threads.
- Use all specified anchors. To achieve tabulated stiffness values, the installation torque for concrete anchors shall be at least 17 ft.-lb. or the torque requirements of the anchor, whichever is greater.
- When using the larger-diameter anchor holes, the bottom track must be predrilled or punched with a ¾"-diameter hole.

Codes: See p. 11 for Code Reference Key Chart

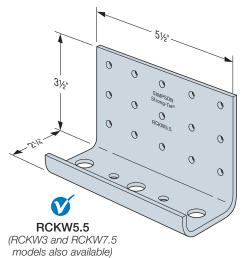
Ordering Information

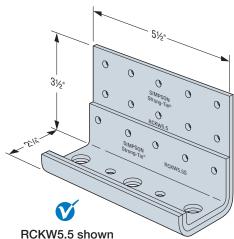
Model No.	Ordering SKU	Dookogo Ougatity
Model No.	Ordering Sko	Package Quantity
RCKW3	RCKW3-R10	10 RCKW3 clips
RCKW5.5	RCKW5.5-R10	10 RCKW5.5 clips
RCKW7.5	RCKW7.5-R10	10 RCKW7.5 clips
RCKW3S	RCKW3S-R10	10 RCKW3S stiffeners
RCKW5.5S	RCKW5.5S-R10	10 RCKW5.5S stiffeners

NEW DESIGN

- Three large holes for added versatility
- Higher capacity option
- Shallowed embedment option







with RCKW5.5S stiffener (RCKW5.5S can also be used with the RCKW7.5; RCKW3S can be used with RCKW3)

US Patent 9,938,709

SIMPSON Strong-Tie



RCKW assembly test with member failure.

Ease of Specification

Many cold-formed steel connector manufacturers provide limited technical data for their products. As a result, designers often rely on detailed and time-consuming hand calculations for CFS connection design. This often involves assumptions regarding connection eccentricity, prying and connection stiffness.

Simpson Strong-Tie strives for ease of specification by providing comprehensive load tables based on tests that simulate real-world conditions. These load tables ensure that tabulated values reflect not only the strength of the connector, but also the strength of the fasteners, the anchorage, the member near the connection, and the overall stiffness. The photo to the right is an example of member failure near the connection. Such failures are reflected in our tabulated loads because of our assembly testing.

Simplified Stiffness Calculations

Some manufacturers tabulate stiffness values only for the connector. It's often unknown or unclear if their stiffness includes the screw fastener slip and how this varies with the thickness of the stud. Additionally, with some manufacturers, the deflection of the stud must be added to the deflection from the rotation of the connector in order to arrive at the final deflection for design.

Because we have tested the entire assembly, Simpson Strong-Tie tabulates stiffness that includes connector deflection, fastener slip and stud deflection for walls up to 38" in height. Our stiffness also takes into account the thickness of the stud, making it simple for the designer to calculate deflections: Simply divide the required moment by the tabulated stiffness, and then multiply the result by the stud length (Ref. Example #1 on p. 107). For walls over 38", a different approach is required (Ref. Example #2 on pp. 108–109).

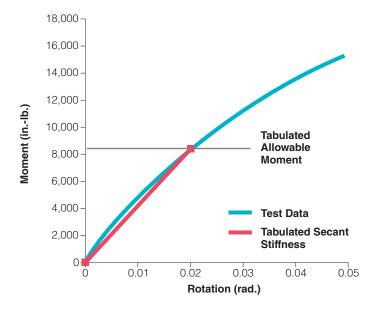




Table 1: RCKW Allowable Loads — Concrete Applications

Model No.	Fastener Pattern No.	Anchor Bolt Dia.	Fasteners to Stud	Framing Members Thickness	Allowable Moment M	Assembly Rotational Stiffness ^{9,11}	Connector Rotational Stiffness ^{10,11} β_{c} (inkip /	Mor (II	lowable nent b.)	Allowable Tension Load F ₂	(II	owable Load, F ₂ o.)	Allowable Shear Load F4	Code Ref.	
		(in.)		mil (ga.)	(inlb.)	(inkip / rad.)	rad.)	f' _C = 3,000 psi	f' _C = 4,000 psi	(lb.)	f' _C = 3,000 psi	f' _C = 4,000 psi	(lb.)		
				33 (20)	2,425	87	93	1,870	1,790	860	1,080	1,055	620		
RCKW3	1	(1) 1/2"	(4) #12	43 (18)	3,080	113	115	2,510	2,355	1,340	1,780	1,705	755		
		(-, ,-	(, ,	54 (16)	4,330	128	137	4,120	3,590	1,850	2,645	2,470	1,120		
				68 (14) 33 (20)	5,150 3,335	141 164	153 175	6,530 ¹⁵	4,570 ¹⁵ 2,590	1,850 1,310	2,645 1,730	2,470 1,665	1,120 620		
RCKW3				43 (18)	4,215	164	175	2,790 3,935	3,465	1,710	2,390	2,250	795		
and RCKW3S	2	(1) 1/2"	(9) #12	54 (16)	5,160	164	175	6,700 ¹⁵	4,585 ¹⁵	2,220	3,410	3,085	1,120		
(stiffener)					68 (14)	5,160	164	175	6,700 ¹⁵	4,58515	2,410	3,875	3,425	1,415	İ
				30 (20 DW) ^{5,6}	3,775	258	280	1,455	1,435	1,030	1,250	1,235	600	ĺ	
				30 (20 STR) ⁶	4,670	260	281	1,830	1,795	1,140	1,395	1,375	665		
	3	(1) 1/2" (6) #12	33 (20)	4,670	304	328	1,830	1,795	1,140	1,395	1,375	665			
		(1) /2	(0) 11 12	43 (18)	6,245	320	338	2,525	2,450	1,440	1,790	1,755	1,035		
				54 (16)	8,225	320	338	3,465	3,320	2,455	3,255	3,125	1,390		
				68 (14)	9,375	417 258	438 280	4,065	3,850 765	2,455 1,030	3,255	3,125 1,235	1,390 600		
				30 (20 DW) ^{5,6} 30 (20 STR) ⁶	3,775 4,670	260	281	770 955	950	1,140	1,250 1,395	1,375	665	l	
			(0)	33 (20)	4,670	304	328	955	950	1,140	1,395	1,375	665	1	
RCKW5.5	3A	(2) 3/8"	(6) #12	43 (18)	6,245	333	355	1,285	1,275	1,440	1,790	1,755	1,035	1	
				54 (16)	8,865	412	439	1,845	1,830	2,455	3,255	3,125	1,390	ĺ	
				68 (14)	11,620	489	519	2,45516	2,42016	2,455	3,255	3,125	1,390	ĺ	
				30 (20 DW) ^{5,6}	3,775	258	280	770	765	1,030	1,250	1,235	600		
3В				30 (20 STR) ⁶	4,670	260	281	955	950	1,140	1,395	1,375	665	ļ	
	3B	(2) 1/2"	(6) #12	33 (20)	4,670	304	328	955	950	1,140	1,395	1,375	665	ļ	
	0.5	(=) /2	` '	43 (18)	6,245	333	355	1,285	1,275	1,440	1,790	1,755	1,035		
				54 (16)	9,995	593	651	2,095	2,070	2,455	3,255	3,125	1,390		
4				68 (14) 33 (20)	11,630 4,855	674 256	734 272	2,460 1,910	2,420 1,870	2,455 1,660	3,255 2,090	3,125 2,040	1,390 665		
				43 (18)	8,445	450	490	3,580	3,420	2,165	2,815	2,720	1,035	l	
	4	(1) 1/2"	(10) #12	54 (16)	11,575	467	502	5,340 ¹⁵	4,93015	2,980	4,115	3,895	1,390		
				68 (14)	14,040	511	513	7,10515	6,27515	2,980	4,115	3,895	1,830	İ	
RCKW5.5				33 (20)	4,855	256	272	990	985	1,660	2,090	2,040	665	IBC,	
and	4A	(2) 3/8"	ś" (10) #12	43 (18)	8,445	450	490	1,755	1,740	2,165	2,815	2,720	1,035	LA	
RCKW5.5S	4/	(2) /8 (10	(<i>-)</i> /0	8 (10)#12	/8 (10) #12	54 (16) 12,920 530 576 2,750 ¹⁶ 2,705 ¹⁶	2,980	4,115	3,895	1,390					
(stiffener)				68 (14)	14,300	626	678	3,06516	3,01016	2,980	4,115	3,895	1,830		
				33 (20)	4,855	256	272	990	985	1,660	2,090	2,040	665		
	4B	(2) 1/2"	1/2" (10) #12	43 (18)	8,445	450 669	490 742	1,755	1,740	2,165	2,815	2,720 3,895	1,035 1,390		
				54 (16) 68 (14)	13,455 16,515	867	966	2,870 3,585	2,820 3,505	2,980 2,980	4,115 4,115	3,895	1,830		
				33 (20)	6,445	389	402	1,815	1,790	1,095	1,315	1,300	795	l	
	_		(0)	43 (18)	8,200	510	536	2,345	2,300	1,280	1,550	1,530	1,200	1	
	5	(1) 1/2"	(6) #12	54 (16)	11,400	554	571	3,370	3,275	2,165	2,715	2,655	1,695	ĺ	
				68 (14)	13,895	605	628	4,225	4,065	2,165	2,715	2,655	1,695		
				33 (20)	6,445	389	402	1,095	1,090	1,095	1,315	1,300	795		
RCKW7.5	5A	(2) 3/8"	(6) #12	43 (18)	8,200	510	536	1,400	1,395	1,280	1,550	1,530	1,200		
11011111110	0,1	(2) /0	(0) 11 12	54 (16)	12,840	820	868	2,23016	2,20516	2,165	2,715	2,655	1,695		
				68 (14)	14,920	912	965	2,61016	2,57516	2,165	2,715	2,655	1,695		
				33 (20)	6,445	389	402	1,095	1,090	1,095	1,315	1,300	795		
	5B	(2) 1/2"	(6) #12	43 (18) 54 (16)	8,200 13,255	510 867	536 927	1,400 2,305	1,395 2,280	1,280 2,165	1,550 2,715	1,530 2,655	1,200 1,695		
				68 (14)	15,640	912	965	2,745	2,705	2,165	2,715	2,655	1,695	l	
				33 (20)	8,705	495	517	2,505	2,450	1,730	2,130	2,095	795		
	_			43 (18)	10,915	591	623	3,210	3,125	2,255	2,840	2,775	1,200	İ	
	6	(1) 1/2"	(10) #12	54 (16)	14,045	689	720	4,275	4,115	2,625	3,360	3,265	1,695	ĺ	
				68 (14)	16,670	689	720	5,245 ¹⁵	4,98515	2,665	3,420	3,320	2,065		
RCKW7.5				33 (20)	8,705	495	517	1,490	1,480	1,730	2,130	2,095	795		
and	6A	(2) 3/8"	(10) #12	43 (18)	10,915	591	623	1,885	1,865	2,255	2,840	2,775	1,200		
RCKW5.5S	UA	(<i>L)</i> 78	(10) #12	54 (16)	17,175	873	930	3,03016	2,98516	2,625	3,360	3,265	1,695		
(stiffener)				68 (14)	18,370	959	1,011	3,25516	3,20016	2,665	3,420	3,320	2,065		
				33 (20)	8,705	495	517	1,490	1,480	1,730	2,130	2,095	795		
	6B	(2) 1/2"	(10) #12	43 (18)	10,915 19,940	591 923	623 991	1,885	1,865	2,255 2,625	2,840	2,775 3,265	1,200		
JB		(), /2		54 (16) 68 (14)	22,555	1,040	1,107	3,550 4,060	3,490 3,975	2,625	3,360 3,420	3,265	1,695 2,065		



RCKW Allowable Load — Concrete Application Footnotes

- 1. For additional important information, see General Information and Notes on p. 22.
- 2. The designer is responsible for anchorage design.
- 3. See illustrations for fastener pattern placement.
- Tabulated values are based on framing members with track and stud of the same thickness and (1) #10 screw into each stud flange unless otherwise noted.
- 5. Tabulated values may be used for framing members with track and stud of thickness 20 mil, $F_V = 57$ ksi (20 EQ).
- 6. Tabulated values are applicable for framing members with CFS track of thickness 20 mil, $F_y = 57$ ksi (20 EQ).
- 7. EQ equivalent, DW drywall, STR structural.
- 8. Tabulated moment values correspond to maximum connector strength without consideration of serviceability, designer must check out-of-plane deflections using tabulated Rotational Stiffness.
- Tabulated Assembly Rotational Stiffness is applicable for walls at 38" tall with corresponding framing member depth and thickness. Reference Example #1 on p. 107.
- 10. Tabulated Connector Rotational Stiffness may be used for any wall heights; the designer must consider member deflection due to bending in the stud member. Reference Example #2 on pp. 108–109.
- 11. Per IBC 2015 Table 1604.3 footnote f, wind load is permitted to be taken as 0.42 times "component and cladding loads" for deflection checks. For IBC 2009 and earlier, the factor is 0.7 instead of 0.42. Tabulated values have not been adjusted.
- 12. Anchor tension, T, is the force in the anchor, or both anchors for two-anchor solutions, at maximum allowable, M, or maximum allowable tension, F₂.
- 13. Tabulated values for anchor tension, T, at allowable tension load, F₂, are provided for total anchor tension for (1) anchor and (2) anchors. See p. 110 for anchorage design tables and illustrations.
- 14. Anchor tension is calculated using AISC Steel Design Guide 1. The 'Anchor Bolt Design' illustration (Figures A and B) shows the anchor tension, T, based on an applied moment, M. An illustration for the anchor tension, T, based on a vertical tension load, F₂, shown in Figure C.
- 15. Tabulated allowable tension loads for the connectors with ½"-diameter anchor bolts require ASTM F3125, Grade A325 or ASTM A449 high-strength bolts. For A307 Grade A bolt, anchor tension load is limited to 4,410 lb.
- 16. Tabulated allowable tension loads for the connectors with %"-diameter anchor bolts require ASTM F3125, Grade A325 or ASTM A449 high-strength bolts. For A307 Grade A bolt, anchor tension load is limited to 2,200 lb.
- 17. Anchor tension, T, may be interpolated.

RCKW3 and RCKW3S Options



RCKW3 Fastener Pattern 1



RCKW3 with RCKW3S Fastener Pattern 2

Bearing pressure

Figure A — Anchor Tension, T, Created from Moment (one anchor)

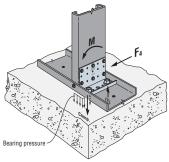


Figure B — Anchor Tension, T, Created from Moment (two anchors)

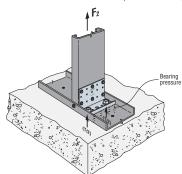


Figure C — Anchor Tension, T, Created from F₂

RCKW5.5 and RCKW5.5S Options



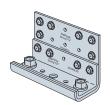
RCKW5.5 Fastener Pattern 3



RCKW5.5 Fastener Pattern 3A, 3B

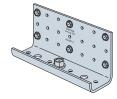


RCKW5.5 with RCKW5.5S Fastener Pattern 4

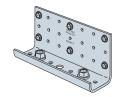


RCKW5.5 with RCKW5.5S Fastener Pattern 4A, 4B

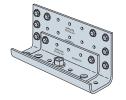
RCKW7.5 and RCKW5.5S Options



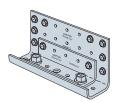
RCKW7.5 Fastener Pattern 5



RCKW7.5 Fastener Pattern 5A, 5B

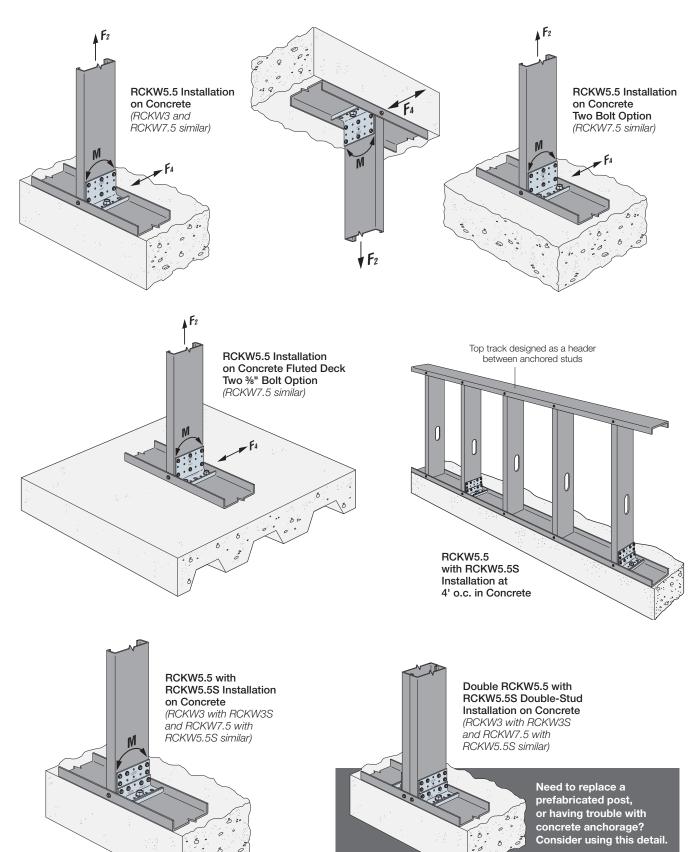


RCKW7.5 with RCKW5.5S Fastener Pattern 6



RCKW7.5 with RCKW5.5S Fastener Pattern 6A, 6B







Example #1: Exterior Parapet Stud

Given:

- 2015 IBC (ASCE 7-10 and AISI S100-2012)
- 600S162-33 (33 ksi) studs @ 16" o.c. supported at the base
- Parapet height, L = 38"-tall studs
- Wind design pressure = 49.67 psf (LRFD)
- Deflection Limits, Δ_{allow} = L/240 (Ref. IBC Table 1604.3)
- 3,000 psi concrete, cracked, SDC A&B, 3" anchor edge

Calculations:

Determine ASD wind pressure:

$$p = (0.6)(49.67 \text{ psf}) = 29.8 \text{ psf}$$

Note: 2015 IBC load combinations for ASD include a factor of 0.6 for wind loads.

$$w = (29.8 \ psf) \frac{16 \ in.}{12 \ in.} = 39.7 \ plf$$

Determine Required Moment:

$$M_{req} = \frac{wL^2}{2} = \frac{(39.7 \, plf)(38 \, in.)^2}{2 \left(12 \frac{in.}{ft.}\right)} = 2,389 \, in.-lb.$$

From Table 1 (p. 104) for 600S162-33,

6"-deep 33-mil stud:

- Select RCKW5.5 connector, fastener pattern 3, with ½" anchor diameter and (6) #12 self-drilling screws, attaching to each stud @ 16" o.c.
- Allowable Moment = 4,670 in.-lb. > 2,389 in.-lb. **OK**
- Assembly Rotational Stiffness, β = 304,000 in.-lb./rad. for RCKW5.5 connector at 38" wall height

Check Deflection at Required Moment:

$$\Delta_{req} = \left(\frac{(0.7)(M_{req})}{\beta}\right) L = \left(\frac{(0.7)(2,389 \text{ in.-lb.})}{304,000 \frac{\text{in.-lb.}}{red}}\right) 38 \text{ in.} = 0.209 \text{ in.}$$

Note: Per IBC Table 1604.3 footnote f, 0.42 factor can be used to calculate deflections for components and cladding wind loads for LRFD loads. ASD load conversion is 0.7.

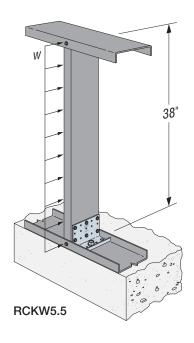
Allowable Deflection:

$$\Delta_{allow} = \frac{2L}{240} = \frac{2(38 \text{ in.})}{240} = 0.317 \text{ in.} > 0.209 \text{ in.}$$
 OK



Computer-Assisted Design Note:

Please use kneewall module in Simpson Strong-Tie® CFS Designer™.



Select Anchorage:

Normal weight concrete with $f'_{\text{C}} = 3,000$ psi Table 2A (p. 111) — Cracked Concrete, Wind and Seismic in SDC A&B

Titen HD® with 31/4" embedment

 $V_a = 39.7*38/12=125.7$ lb.

 $N_a = 2,389/4,670*1,830 = 936$ (interpolate from Table 1 (p. 104))

 $V_{al} = 930^{\circ}0.86 = 799.8$

 $N_{al} = 1,335*0.86 = 1,148.1$

*Note: 0.86 comes from note 11, Table 2A (p. 112) (3,000 psi concrete)

 $V_a/V_{al} = 125.7/799.8 = 0.16 < 1$ **OK**

 $N_a/N_{al} = 936/1,148.1 = 0.82 < 1$ **OK**

Interaction = 0.16 + 0.82 = 0.98 < 1.2 **OK**



Example #2: High Interior Half-Wall — Concrete Slab, No Edge, Two Anchor

Given:

- 2015 IBC (ASCE 7-10 and AISI S100-2012)
- The top track 600T125-54 (50 ksi) spans between 600S162-54 (50 ksi) studs @ spacing, S = 32" o.c. supported at the base
- 6" drywall studs at 16" o.c. as infill between the bottom and top track
- Wall height, L = 48"-tall studs
- Design Load: w = 50 plf or P = 200 lb. concentrated load for guard or handrail applications in accordance with Section 4.5.1 of ASCE (Ref. IBC 1607.8.1 and 1607.8.1.1)
- Deflection Limit, $\Delta_{allow} = L/120$ (Ref. IBC Table 1604.3)
- 4,000 psi NWC, uncracked A&B, no edge, 5" concrete thickness

Calculations:

Design criteria #1 for linear load of 50 lb./ft. Determine Required Concentrated Load, Preq:

$$P = (w)(S) = (50 \text{ plf})(32 \text{ in.}) \left(\frac{1 \text{ ft.}}{12 \text{ in.}}\right) = 133.3 \text{ lb.}$$

Determine Required Moment, Mreq:

$$M_{reg} = (P_{reg})(L) = (133.3 \text{ lb.})(48 \text{ in.}) = 6,400 \text{ in.-lb.}$$

Design criteria #2 for concentrated load of 200 lb.

Note: From a 3D structural analysis with the 200 lb. concentrated load at the end stud, a continuous top track distributes some load to adjacent studs so that the worst-case moment is $M_{\text{req(max)}} = 7,513$ in.-lb. and maximum shear is $V_{\text{req(max)}} = 157$ lb. as indicated in the illustration.

From Table 1 (p. 104) for 600S162-54, 6"-deep, 54-mil stud:

- Select a RCKW5.5 connector, screw pattern 3B with (6) #12 self-drilling screws and (2) ½"-diameter anchors
- Allowable Moment = 9,995 in.-lb. > 6,400 in.-lb. (for linear load) **OK**
- Allowable Moment = 9,995 in.-lb. > 7,513 in.-lb. (for concentrated load) **OK**
- Connector Rotational Stiffness $\beta_C = 651,000$ in.-lb. / rad.

Check Deflection for Design Criteria #1 at Required Load:

Determine Stud Deflection, Δ_s , at $P_{req} = 133.3$ lb.

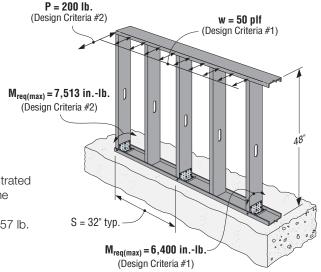
$$\Delta_{S} = \frac{P_{req}L^{3}}{3EI_{xe}} = \left(\frac{(133.3 \text{ lb.})(48 \text{ in.})^{3}}{3(29,500,000 \text{ psi})(2.86 \text{ in.}^{4})}\right) = 0.058 \text{ in.}$$

Note: Effective moment of inertia for a 600S162-54 stud is $I_{xe} = 2.86$ in.⁴

Determine Connector Deflection, Δ_c , at $M_{req} = 6,400$ in.-lb. by utilizing the Connector Rotational Stiffness, $\beta_c = 651,000$ in.-lb. / rad. for RCKW5.5.

$$\Delta_C = \frac{M_{req}}{\beta_C} L = \frac{6,400 \text{ in.-lb.}}{651,000 \frac{\text{in.-lb.}}{rad}} (48 \text{ in.}) = 0.472 \text{ in.}$$

Note: The Connector Rotational Stiffness may be used for any wall height; the designer must consider member deflection due to bending in the stud member. See footnote 10 of Table 1 (p. 105).



RCKW5.5 Installation on Concrete

SIMPSON Strong-Tie

Example #2: High Interior Half-Wall — Concrete Slab, No Edge, Two Anchor (cont.)

Total Deflection is the sum of the Stud Deflection and the Connector Deflection.

$$\Delta_{total} = \Delta_{S} + \Delta_{C} = 0.058 \text{ in.} + 0.472 \text{ in.} = 0.53 \text{ in.}$$

Allowable Deflection:

$$\Delta_{allow} = \frac{2L}{120} = \frac{(2)(48 \text{ in.})}{120} = 0.800 \text{ in.} > 0.53 \text{ in.}$$
 OK

Check Deflection for Design Criteria #2 at Required Load:

Determine Stud Deflection, Δ_s , at $M_{req} = 7,513$ in.-lb. from concentrated load.

$$\Delta_S = \frac{M_{req}L^2}{3EI_{Xe}} = \left(\frac{(7,513 \text{ in.-lb.})(48 \text{ in.})^2}{3(29,500,000 \text{ psi})(2.86 \text{ in.}^4)}\right) = 0.068 \text{ in.}$$

Determine Connector Deflection, Δ_c , at M_{req} = 7,513 in.-lb. by utilizing the Connector Rotational Stiffness, β_c = 651,000 in.-lb. / rad. for RCKW5.5.

$$\Delta_C = \frac{M_{req}}{\beta_C} L = \frac{7,513 \text{ in.-lb.}}{651,000 \frac{\text{in.-lb.}}{rad.}}$$
 (48 in.) = 0.554 in.

Total Deflection is the sum of Stud Deflection and Connector Deflection.

$$\Delta_{total} = \Delta_{s} + \Delta_{c} = 0.068 \text{ in.} + 0.554 \text{ in.} = 0.622 \text{ in.}$$

Allowable Deflection:

$$\Delta_{allow} = \frac{2L}{120} = \frac{(2)(48 \text{ in.})}{120} = 0.800 \text{ in.} > 0.622 \text{ in.}$$
 OK

Select Anchorage:

Normal-weight concrete with f'c = 4,000 psi

Table 2A (p. 110) — Uncracked Concrete Wind and Seismic in SDC A&B (2) $\frac{1}{2}$ "-diameter Titen HD® with $3\frac{1}{4}$ " embedment $V_a = 157$ lb.

 $V_{\text{al}} = 3,765$ lb. Table 2A (p. 9) two anchors assumed to act in shear with no edge condition.

$$V_a/V_{al} = 157 \text{ lb./3,765 lb.} = 0.04 < 1 \text{ OK}$$

Interpolation of N_a , anchor tension, at M = 7,513 in.-lb.

 $N_a = 7,513/9,995*2,070 = 1,556$ lb. Table 1 (p. 104)

 $N_{al} = 2,130$ lb. Table 2A (p. 110) Only one-anchor acts in tension with no edge condition.

 $N/N_{al} = 1,556 \text{ lb.} / 2,130 \text{ lb.} = 0.73 < 1 \text{ OK}$

Interaction = 0.04 + 0.73 = 0.77 < 1.2 **OK**

Note: Per ASCE Section 4.5.1, for handrail and guardrail systems, there is no need to apply the 50 plf linear load and the 200 lb. concentrated load concurrently. Example #2 demonstrates the design for both loading cases, and the outermost anchored stud governs when using the 200 lb. concentrated load.



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Computer-Assisted Design Note:

Please use kneewall module in Simpson Strong-Tie® CFS Designer™.



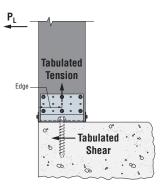


Figure 2A-1 Single Anchor — One Anchor Shear, One Anchor Tension (tension from moment created from P_I)

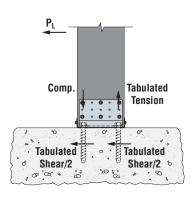


Figure 2A-2 Two Anchors — Two Anchors Shear, One Anchor Tension (tension from moment created from P_I)

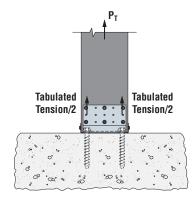


Figure 2A-3 Two Anchors — Two Anchors Tension (tension created from P_T)

Table 2A: RCKW Allowable Tension and Shear Loads Using 1/2"-Diameter Anchor

							All	owable Ten	sion and SI	near Load (lb.)			
Model No.		Load Type	No. of ½"- Diameter Anchor	Titen HD®	Titen HD	Strong- Bolt® 2	AT-XP®	SET-XP®	SET-3G™	SET-XP	SET-3G	AT-XP	SET-XP	SET-3G
(Min. Anchor	Type of Concrete						Mir	nimum Con	crete Thick	ness, h _{min}	(in.)			
Edge Distance)	Control	Туро	(Acting in Load Type	5	6	6	6	6	6	6½	6½	9½	9½	9½
			Indicated)		Nominal Embedment Depth, h _{nom} (in.)									
				31/4	3¾	37/8	3½	3½	4¾	4	51/4	7	7	81⁄4
			U	ncracked C	oncrete, W	ind and Sei	smic in SD	C A and B ^{8,}	$^{\circ}$ (f' _C = 4,00	0 psi)				
	SLWC	Tension	1	815	910	_	435	525	525	_	_	_	_	_
RCKW3	SLWC	Shear	1	410	425	_	445	445	455	_	_	_	_	_
(Edge = 11/8")	NWC	Tension	1	1,200	1,340		855	960	1,005	_	_	_	_	_
		Shear	1	605	625	_	655	655	675	_	_	_	_	_
	SLWC	Tension	1	1,270	1,465		655	780	760	_	_	_	_	_
RCKW5.5		Shear	1	815	915	_	960	960	985	_	_	_	_	_
(Edge = 3")	NWC	Tension	1	1,865	2,150	_	1,280	1,495	1,435	_	_	_	_	_
		Shear	1	1,305	1,350	_	1,410	1,410	1,450	_	_	_	_	_
	SLWC	Tension	1	1,450	1,800	1,415	875	1,025	995	_	_	_	_	_
RCKW7.5		Shear	1	1,245	1,410	1,465	1,480	1,480	1,520	_	_	_	_	_
(Edge = 4")	NWC	Tension	1	2,130	2,645	2,080	1,720	1,925	1,870	_	_	_	_	_
	INVVC	Shear	1	1,830	2,075	2,160	1,880	1,880	1,925	_	_	_	_	_
		Tension	1	1,450	1,865	1,765	1,470	1,830	2,815	2,090	3,110	2,940	3,660	3,705
	SLWC	161121011	2	2,375	2,875	3,525	2,020	2,445	3,730	2,795	4,120	4,045	4,890	6,480
	SLWC	Shear	1	1,560	2,685	2,820	1,925	1,925	1,925	1,925	1,925	1,925	1,925	1,925
RCKW All models		Sileai	2	2,560	5,370	5,645	3,855	3,855	3,855	3,855	3,855	3,855	3,855	3,855
(no edge)		Tension	1	2,130	2,745	2,595	2,885	3,355	3,705	3,705	3,705	3,705	3,705	3,705
	NWC	TELISION	2	3,495	4,225	5,185	3,965	4,795	6,985	5,475	7,410	7,410	7,410	7,410
	INVVC	Shear	1	2,295	2,685	2,820	1,925	1,925	1,925	1,925	1,925	1,925	1,925	1,925
		Sileai	2	3,765	5,370	5,645	3,855	3,855	3,855	3,855	3,855	3,855	3,855	3,855

Table continued on next page.

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Table 2A: RCKW Allowable Tension and Shear Loads Using 1/2"-Diameter Anchor (cont.)

10010 27	Type of Concrete	Load Type	No. of ½"- Diameter Anchor (Acting in Load Type Indicated)		Allowable Tension and Shear Load (lb.)										
Model No.				Titen HD®	Titen HD	Strong- Bolt® 2	AT-XP®	SET-XP®	SET-3G™	SET-XP	SET-3G	AT-XP	SET-XP	SET-3G	
(Min. Anchor Edge Distance)							Mir	nimum Con	crete Thick	ness, h _{min}	(in.)				
				5	6	6	6	6	6	6½	6½	91/2	9½	9½	
,							No	minal Emb	edment De	pth, h _{nom} (in.)				
				31/4	3¾	37/8	3½	3½	43/4	4	51/4	7	7	81/4	
				Cracked Co	ncrete, Wir	nd and Seis	mic in SDC	A and B ^{8,10}	(f' _C = 4,000) psi)					
		Tension	1	585	645	_	355	_	585	320	645	710	560	1,015	
RCKW3	SLWC	Shear	1	295	305	_	320	_	325	325	325	325	325	325	
(Edge = 17/8")	AUMO	Tension	1	860	950	_	700	_	1,145	630	1,265	1,395	1,100	1,985	
	NWC	Shear	1	430	445	_	465	_	480	480	480	480	480	480	
	CLWC	Tension	1	910	1,040	_	535	_	840	465	930	1,065	815	1,460	
RCKW5.5	SLWC	Shear	1	635	655	_	685	_	705	705	705	705	705	705	
(Edge = 3")	NIMO	Tension	1	1,335	1,530	_	1,045	_	1,650	915	1,820	2,090	1,600	2,815	
	NWC	Shear	1	930	965		1,010		1,035	1,035	1,035	1,035	1,035	1,035	
	SLWC	Tension	1	1,025	1,280	1,255	715		1,100	615	1,220	1,435	1,075	1,915	
RCKW7.5	SLWC	Shear	1	890	1,010	1,050	1,055	_	1,085	1,085	1,085	1,085	1,085	1,085	
(Edge = 4")	NWC	Tension	1	1,510	1,880	1,845	1,405	_	2,160	1,205	2,390	2,810	2,110	3,370	
	INVVO	Shear	1	1,310	1,485	1,540	1,550		1,595	1,595	1,595	1,595	1,595	1,595	
	Tension	1	1,025	1,320	1,255	960		1,710	925	1,890	1,915	1,615	2,970		
	SLWC	101131011	2	1,685	2,035	2,505	1,315	_	2,265	1,240	2,505	2,630	2,170	3,940	
	SLWO	Shear	1	1,105	2,465	2,820	1,925		1,925	1,925	1,925	1,925	1,925	1,925	
RCKW All models		Oncai	2	1,815	4,380	5,500	3,350	_	3,855	3,155	3,855	3,855	3,855	3,855	
(no edge)		Tension	1	1,510	1,945	1,845	1,880	_	3,355	1,810	3,705	3,705	3,170	3,705	
	NWC	101101011	2	2,475	2,990	3,685	2,580	_	4,445	2,430	4,915	5,160	4,250	7,410	
	IVVO	Shear	1	1,625	2,685	2,820	1,925		1,925	1,925	1,925	1,925	1,925	1,925	
		Onour	2	2,665	5,370	5,645	3,855	_	3,855	3,855	3,855	3,855	3,855	3,855	
				Cracked	Concrete,	Seismic in S	SDC C Thro	ugh F ^{9,10} (f' ₀	c = 4,000 p	si)					
	SLWC	Tension	1	205	225	_	105	_	185	110	205	210	195	320	
RCKW3	OLWO	Shear	1	135	140	_	150	_	150	150	150	150	150	150	
(Edge = 1%")	NWC	Tension	1	300	335	_	210	_	360	220	400	415	385	625	
	11110	Shear	1	200	210		220		225	225	225	225	225	225	
	SLWC	Tension	1	320	365		160		265	165	295	315	285	460	
RCKW5.5		Shear	1	295	305	_	320	_	330	330	330	330	330	330	
(Edge = 3")	NWC	Tension	1	470	535	_	310	_	520	320	575	620	560	900	
		Shear	1	435	450	_	470	_	485	485	485	485	485	485	
	SLWC	Tension	1	360	450	440	215		345	215	385	425	375	605	
RCKW7.5		Shear	1	415	470	490	495	_	505	505	505	505	505	505	
(Edge = 4")	NWC	Tension	1	530	660	645	420		680	420	750	835	740	1,180	
		Shear	1	610	690	720	725		675	700	675	745	700	675	
		Tension	1	360	465	440	285	_	540	325	595	570	565	935	
	SLWC		2	590	710	875	390	_	715	435	790	785	760	1,240	
DCKW		Shear	1	515	805	1,185	765	_	675	700	675	765	700	675	
RCKW All models			2	845	1,610	2,225	1,330	_	1,350	1,405	1,350	1,530	1,405	1,350	
(no edge)		Tension	1	530	680	645	560	_	1,055	635	1,170	1,115	1,110	1,730	
	NWC		2	865	1,045	1,290	770	_	1,400	850	1,550	1,535	1,490	2,435	
		Shear	1	760	805	1,185	765	_	675	700	675	765	700	675	
		Silear	2	1,245	1,610	2,370	1,530		1,350	1,405	1,350	1,530	1,405	1,350	

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Rigid Connectors

RCKW Kneewall Connectors

Table 2B: RCKW Allowable Tension and Shear Loads Using (2) %"-Diameter Anchors

				Allowable	Tension and Shear	Load (lb.)			
		Load Type	No. of	Titen HD®	Strong-Bolt® 2	SET-3G™			
Model No. (Min.			%"- Diameter	Minimum Concrete Thickness, h _{min} (in.)					
Anchor Edge Distance)	Type of Concrete		Anchor (Acting in Load Type Indicated)	4 Slab and 3¼ Top of Metal Deck	4	4			
				Nominal	Embedment Depth,	h _{nom} (in.)			
				21/2	21/4	2¾			
	Uncrack	ed Concrete	e, Wind and Sei	ismic in SDC A and	$B^{8,10}$ (f' _c = 4,000 psi)				
		Tension -	1	905	885	1,410			
	SLWC		2	1,750	1,765	2,010			
RCKW5.5 RCKW7.5		Shear	1	1,020	700	1,060			
(no edge)		Tension -	1	1,330	1,300	2,035			
(3 - /	NWC		2	2,575	2,595	3,935			
		Shear	1	1,500	700	1,060			
	Cracked	d Concrete,	Wind and Seis	mic in SDC A and B	8,10 (f' _c = 4,000 psi)				
		Tension -	1	415	620	820			
	SLWC		2	830	1,245	1,170			
RCKW5.5 RCKW7.5		Shear	1	725	700	1,060			
(no edge)		Tension	1	610	915	1,610			
	NWC	161191011	2	1,220	1,830	2,295			
		Shear	1	1,065	700	1,060			
	Crac	ked Concre	te, Seismic in	SDC C Through F ^{9,10}	(f' _c = 4,000 psi)				
		Tanaiar	1	145	220	290			
	SLWC	Tension	2	290	435	410			
RCKW5.5		Shear	1	335	330	370			
RCKW7.5 (no edge)		Tension	1	215	320	565			
	NWC	161191011	2	425	640	805			
		Shear	1	480	330	370			

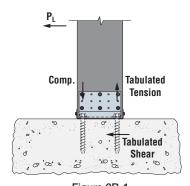


Figure 2B-1 Two Anchors - One Anchor Shear**, One Anchor Tension

(tension from moment created from P_I) **One anchor acting in shear due to 3/8" anchor in larger hole.

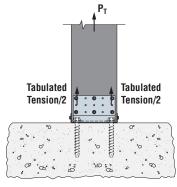


Figure 2B-2 Two Anchors - Two Anchors Tension (tension created from P_T)

Table 2A and 2B Notes:

- 1. Anchor Allowable Loads have been determined using ACI 314-14 Chapter 17 anchorage calculations with the minimum concrete compressive strength, f'c, and slab thickness listed. Sand-Lightweight Concrete is abbreviated as 'SLWC', Normal Weight Concrete is abbreviated as 'NWC'.
- Load values are for anchor based on ACI 318-14, condition B, load factors from ACI 318 Section 5.3, no supplemental edge reinforcement, Ψ_{C,V} = 1.0 for cracked concrete and periodic special inspection. Reference ICC-ES or IAPMO-UES evaluation reports for further information.
- Load values are based on short-term temperature range of 150°F, 160°F and 180°F for SET-XP®, SET-3G and AT-XP® adhesives, respectively. Long-term temperature range is assumed to be 110°F for SET-XP, SET-3G and AT-XP adhesives.
- 4. Allowable Stress Design (ASD) values were determined by multiplying calculated Strength Design values by a conversion factor, Alpha (α), of 0.7 for seismic loads and 0.6 for wind loads. ASD values for other load combinations may be determined using alternate conversion factors.
- 5. End distances are assumed as 1.5 x Min. Edge Distance in one direction and 'N/A' in the other direction. See figure on this page.
- 6. Edge and end distances are assumed as 'N/A' in all directions at locations for (No Edge).
- 7. Tabulated anchorage capacities for RCKW models shown are applied to the same model size with stiffener. For example, a value for model RCKW3 is equivalent to model RCKW3 and RCKW3S
- Tabulated allowable ASD loads for Wind and Seismic in SDC A and B are based on using wind conversion factors and may be increased by 1.17 for seismic SDC A and B only.
- Allowable loads have been divided by an Omega (Ω) seismic factor of 2.5 for brittle failure as required by ACI 318-14 Chapter 17, unless steel failure governs.
- 10. Tabulated capacities are based on maximum allowable anchorage loads only. The capacity of the connection system shall be the minimum of the tabulated value and the RCKW allowable load value listed on p. 104.
- 11. Tabulated loads in Tables 2A and 2B are based on $f'_{C} = 4,000$ psi. For f'_C = 3,000 psi, use an adjustment factor of 0.86 for the blue shaded values and 1.0 for all other values.
- 12. For anchor subjected to both tension and shear loads,
 - it shall be designed to satisfy following:

 - For N_a / N_{al} \leq 0.2, the full allowable load in shear is permitted. For V_a / V_{al} \leq 0.2, the full allowable load in tension is permitted.
 - For all other cases: $N_a / N_{al} + V_a / V_{al} \le 1.2$.

where:

Na = Applied ASD tension load

Nal = Allowable tension load from Table 2A or 2B

Va = Applied ASD shear load

Val = Allowable shear load from Table 2A or 2B.

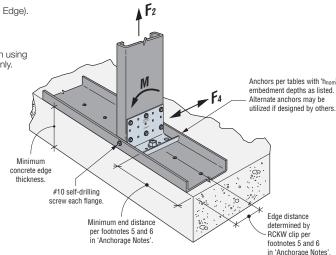
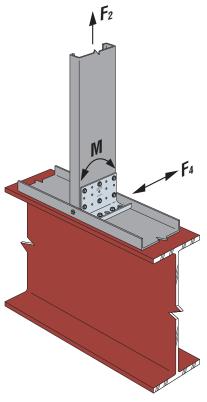




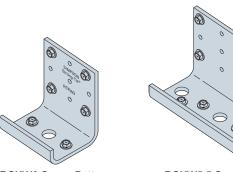
Table 3: RCKW Allowable Loads — Steel Applications with Anchorage

Model No.	Framing Member Depth (in.)	Fastener to Structural Steel ²	Fastener to Stud ³	Framing Member Thickness mil (ga.)	Allowable Moment ^{4,5} M (inlb.)	Assembly Rotational Stiffness ^{6,8} B (inlb./rad)	Connector Rotational Stiffness ^{7,8} $\beta_{\rm C}$ (inlb./rad)	Allowable Tension Load F ₂ (lb.)	Allowable Shear Load F4 (lb.)	Code Ref.
RCKW3 3.62				33 (20)	2,105	55,500	58,000	850	455	
	3.625	(2) #12	(4) #12	43 (18)	2,570	73,300	76,700	1,225	745	
				54 (16)	2,690	87,260	91,200	1,115	1,115	
		(4) #12	(6) #12	33 (20)	5,165	199,200	209,200	1,245	650	
RCKW5.5	6.00			43 (18)	6,370	272,600	287,100	1,900	1,060	_
				54 (16)	6,430	255,900	266,100	2,000	1,295	
				33 (20)	7,030	456,700	483,200	965	655	
RCKW7.5	8.00	(6) #12	(6) #12	43 (18)	9,595	571,600	603,600	1,950	1,135	
				54 (16)	11,320	693,600	731,600	2,185	1,710	

- 1. For additional important information, see General Information and Notes on p. 22.
- 2. Designer is responsible for structural steel design.
- 3. See illustrations for fastener patterns.
- 4. Tabulated values are based on framing members with track and stud of the same thickness and #10 screws into each stud flange.
- 5. Tabulated moment values correspond to the maximum connector strength without consideration of serviceability. Designer must check out-of-plane deflections using tabulated Rotational Stiffness.
- 6. Tabulated Assembly Rotational Stiffness is for walls at 38" tall.
- 7. The tabulated Connector Rotational Stiffness is for any wall heights. The designer must consider member deflection due to bending in the stud.
- 8. Per IBC 2015 Table 1604.3 footnote f, wind load is permitted to be taken as 0.42 times "component and cladding loads" for deflection checks. For IBC 2009 and earlier, the factor is 0.7 instead of 0.42.

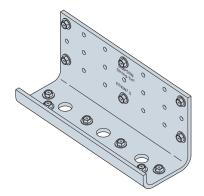


RCKW5.5 Installation on Structural Steel (RCKW3 and RCKW7.5 similar)



RCKW3 Screw Pattern for Steel Anchorage

RCKW5.5 Screw Pattern for Steel Anchorage

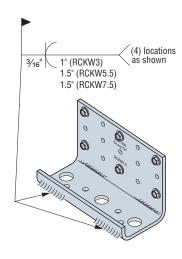


RCKW7.5 Screw Pattern for Steel Anchorage

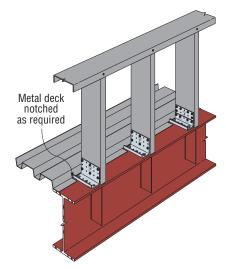


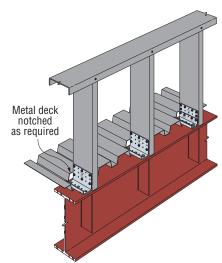
Table 4: RCKW Allowable Loads — Steel Applications with Bolted or Welded Anchorage

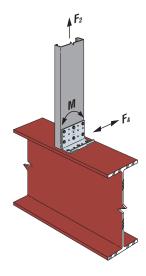
Model No.	Fastener Pattern No.	Anchor Bolt Diameter or Weld to Structural Steel	Fasteners to Stud	Framing Members Thickness mil (ga.)	Allowable Moment M (inlb.)	Assembly Rotational Stiffness ^{6,8} β (inkip/rad.)	Connector Rotational Stiffness ^{7,8} $\beta_{\rm C}$ (inkip/rad.)	Allowable Tension Load F ₂ (lb.)	Allowable Shear Load F4 (lb.)
				33 (20)	2,425	87	93	860	620
RCKW3	1	(1) ½"	(4) #12	43 (18)	3,080	113	115	1,340	755
nunwa	'	or (4) 1" weld	(4) #12	54 (16)	4,330	128	137	1,850	1,120
		(1) 1 11010		68 (14)	5,150	141	153	1,850	1,120
RCKW3				33 (20)	3,335	164	175	1,310	620
and		(1) 1/."	(9) #12	43 (18)	4,215	164	175	1,710	795
RCKW3S	4	(1) 1/2"	(9) #12	54 (16)	5,160	164	175	2,220	1,120
(stiffener)				68 (14)	5,160	164	175	2,410	1,415
				33 (20)	4,670	304	328	1,140	665
	3	(1) ½"	(6) #12	43 (18)	6,245	320	338	1,440	1,035
	3			54 (16)	8,225	320	338	2,455	1,390
RCKW5.5 -				68 (14)	9,375	417	438	2,455	1,390
		(2) ½" or (4) 1½" weld		33 (20)	4,670	304	328	1,140	665
	3B		(6) #12	43 (18)	6,245	333	355	1,440	1,035
				54 (16)	9,995	593	651	2,455	1,390
		(1) 1/2 Wold		68 (14)	11,630	674	734	2,455	1,390
				33 (20)	4,855	256	272	1,660	665
		(1) 1/2"	(40) #40	43 (18)	8,445	450	490	2,165	1,035
RCKW5.5	4	(1) 72	(10) #12	54 (16)	11,575	467	502	2,980	1,390
and				68 (14)	14,040	511	513	2,980	1,830
RCKW5.5S	4B	(2) ½"	(10) #12	33 (20)	4,855	256	272	1,660	665
(stiffener)				43 (18)	8,445	450	490	2,165	1,035
				54 (16)	13,455	669	742	2,980	1,390
				68 (14)	16,515	867	966	2,980	1,830
				33 (20)	6,445	389	402	1,095	795
	5	(4) 1/11	(0) 1146	43 (18)	8,200	510	536	1,280	1,200
	5	(1) ½"	(6) #12	54 (16)	11,400	554	571	2,165	1,695
RCKW7.5				68 (14)	13,895	605	628	2,165	1,695
norwii.5				33 (20)	6,445	389	402	1,095	795
	5B	(2) 1/2"	(6) #12	43 (18)	8,200	510	536	1,280	1,200
) DD	or (4) 1½" weld	(0) #12	54 (16)	13,255	867	927	2,165	1,695
		(1) 1/2 Wold		68 (14)	15,640	912	965	2,165	1,695
				33 (20)	8,705	495	517	1,730	795
	E	(1) 1/-	(10) #10	43 (18)	10,915	591	623	2,255	1,200
RCKW7.5	6	(1) 1/2"	(10) #12	54 (16)	14,045	689	720	2,625	1,695
and				68 (14)	16,670	689	720	2,665	2,065
RCKW5.5S				33 (20)	8,705	495	517	1,730	795
(stiffener)	6B	(2) 1/-!!	(10) #10	43 (18)	10,915	591	623	2,255	1,200
	OB	(2) 1/2"	(10) #12	54 (16)	19,940	923	991	2,625	1,695
				68 (14)	22,555	1,040	1,107	2,665	2,065



- 1. For additional important information, see General Information and Notes on p. 22.
- 2. Designer is responsible for structural steel design.
- 3. See illustrations on p. 105 for stud fastener patterns. For weld pattern to steel beam, see illustration above.
- 4. Tabulated values are based on framing members with top track and stud of the same thickness and #10 screws into each stud flange.
- 5. Tabulated moment values correspond to the maximum connector strength without consideration of serviceability. Designer must check out-of-plane deflections using tabulated Rotational Stiffness.
- Tabulated Assembly Rotational Stiffness is for wall at 38" tall.
- The tabulated Connector Rotational Stiffness is for any wall heights. The designer must consider member deflection due to bending in the stud.
- Per IBC 2015 Table 1604.3 footnote f, wind load is permitted to be taken as 0.42 times "component and cladding loads" for deflection checks. For IBC 2009 and earlier, the factor is 0.7 instead of 0.42.







Rigid Connectors